

# Defect profile and microstructural development in SnO<sub>2</sub>-based varistors

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## Abstract

The microstructural development and the stabilised valence of the ions added to SnO<sub>2</sub> were analysed. Aiming at a better interpretation of the involved phenomena, the effects on grain growth, secondary phase formation and structure of adding Co<sub>3</sub>O<sub>4</sub>, ZnO, MnO<sub>2</sub>, Sb<sub>2</sub>O<sub>3</sub>, or Nb<sub>2</sub>O<sub>5</sub> have been studied. We found that cobalt, zinc and manganese stabilise as Co<sup>+2</sup>, Zn<sup>+2</sup> and Mn<sup>+2</sup> in the lattice, favouring the oxygen vacancy apparition and then, the grain growth and the potential barrier formation. Sb<sub>2</sub>O<sub>3</sub> or Nb<sub>2</sub>O<sub>5</sub> reduces the total oxygen vacancy concentration and the grain growth. Sb<sub>2</sub>O<sub>3</sub> addition favours the CoSnO<sub>3</sub> particle formation and Nb<sub>2</sub>O<sub>5</sub> favours the formation of particles with an intermediate composition between CoSnO<sub>3</sub> and Co<sub>2</sub>SnO<sub>4</sub> in systems with Co<sub>3</sub>O<sub>4</sub>. These particles could also control the sintering and grain growth rates.

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## 1. Introduction

Varistors are semiconductor devices whose current–voltage characteristics are highly non-linear. Their primary function is to sense and limit transient voltage surges and to do so repeatedly without being destroyed.<sup>1,2</sup> The non-linear current–voltage (*I–V*) characteristic is expressed by the equation  $I = V^\alpha$ , where  $\alpha$  is the non-linearity coefficient.<sup>3</sup> Ohmic resistors have  $\alpha = 1$  while ideal varistors have infinite values of  $\alpha$ .

Commercial varistors are based on SiC or in ZnO. SiC based varistors have very low non-linearity coefficient ( $\alpha = 5$ ) while ZnO-based varistors have very high non-linearity coefficient ( $\alpha = 50$ ).<sup>4</sup> At the same time, other varistor systems have been studied, because of the need for even better properties. Among them, systems based on SrTiO<sub>3</sub>,<sup>5</sup> TiO<sub>2</sub>,<sup>6,7</sup> and SnO<sub>2</sub><sup>8–10</sup> have been described in the literature.

Tin oxide is a semiconductor with crystalline structure of rutile type and has very low densification rate due to its high surface diffusion at low temperatures and high SnO<sub>2</sub> partial pressure at high temperatures.<sup>11</sup> Due to this particular property, SnO<sub>2</sub> has been extensively used

as gas sensors.<sup>12,13</sup> Pianaro et al.<sup>8</sup> reported that doping by Co<sub>2</sub>O<sub>3</sub> and Nb<sub>2</sub>O<sub>5</sub> drastically improve the sinterability of SnO<sub>2</sub>, and they observed highly non-linear current–voltage characteristic. At present it is known that several dopants (such as CoO, MnO<sub>2</sub>) form solid solutions with SnO<sub>2</sub> and create charged oxygen vacancies at sintering temperatures. These oxygen vacancies as well as Mn<sup>+2</sup>, Mn<sup>+3</sup> or Co<sup>+2</sup> ions substituting Sn<sup>+4</sup> are segregated at the grain boundaries and improve mass transport leading to densification and grain growth.<sup>14</sup> Other additives (such as Bi<sub>2</sub>O<sub>3</sub> and CuO) improve SnO<sub>2</sub> densification by forming a reactive liquid phase.<sup>10,15</sup> On the other hand, it was reported that Sb<sub>2</sub>O<sub>3</sub> or Nb<sub>2</sub>O<sub>5</sub> decreases the SnO<sub>2</sub> sinterability.<sup>16,17</sup>

The goal of the present work is to investigate the influence of Co<sub>3</sub>O<sub>4</sub>, ZnO, MnO<sub>2</sub>, Sb<sub>2</sub>O<sub>3</sub>, Nb<sub>2</sub>O<sub>5</sub> on the microstructure development, on the secondary phases formation, on the lattice volume, on the defect structure, and on the electrical behaviour. Also, the stabilised valence of the ions added in the SnO<sub>2</sub> lattice is analysed.

## 2. Experimental procedure

Analytical grades of SnO<sub>2</sub> (Aldrich, average particle size 0.42  $\mu\text{m}$ , specific area 5.5 m<sup>2</sup>/g), Co<sub>3</sub>O<sub>4</sub> (Merck),

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ZnO (Mallinckrodt), MnO<sub>2</sub> (Merck), Sb<sub>2</sub>O<sub>3</sub> (Carlo Erba), Nb<sub>2</sub>O<sub>5</sub> (Fluka AG), were used as precursors for processing SnO<sub>2</sub> based varistors. Selected compositions are listed in Table 1. Starting powders were mixed in alcoholic medium by stirring in a high-speed turbine at 6000 rpm for 5 min. Then, slurries were dried at 65 °C until constant weight. After being cooled down, mixtures were crushed into powder and sieved through a 43 µm mesh screen. Finally, samples were pressed (200 MPa) into disks of 1 cm in diameter and 0.15 cm thick. They were sintered at 1300 °C for 2 h (heating and cooling rate: 3 °C/min).

In order to calculate the apparent density of the sintered samples, Archimedes method was applied. Microstructural characteristics of the polished and thermally etched samples were observed by scanning electron microscopy (SEM) using a Philips 505 microscope, while elemental analyses (EDS) were carried out with an EDAX (Topcon SM-300 and PGT digital spectrometer). By using the Soft Imaging System AnalySIS<sup>®</sup> 3.0 software, evaluation of the average grain size was performed on SEM images. X-ray diffraction (XRD) analysis of the SnO<sub>2</sub> was carried out on sintered samples, using a Philips PW 1050/25 equipment with CuK<sub>α</sub> radiation and a Ni filter, at 40 kV and 30 mA. From XRD reflections corresponding to the (110) and (101) planes, a qualitative analysis of the cell distortion in SnO<sub>2</sub> samples was made. These signals were located in a value of the 2θ angle (radiation CuK<sub>α</sub>) ≈ 26.61° [(110) plane] and 2θ ≈ 33.89° [(101) plane]. The spacings (*d*<sub>1</sub> and *d*<sub>2</sub>) of the crystallographic planes [(110) and (101)] were determined using the Bragg condition. To quantify the cell distortion, *c* and *a* parameters for the tetragonal system were calculated with the following equations:<sup>18</sup>

$$1/d_1 = 2/a^2 \quad (1)$$

$$1/d_2 = 1/a^2 + 1/c^2 \quad (2)$$

To achieve a precise data collection, scanning was performed at 0.125°/min and 2θ angle ranging from 26 to 28° and from 33 to 35°.

A Bruker ER-200 (Band X) EPR spectroscope with a variable gain between 2 × 10<sup>4</sup> and 8 × 10<sup>3</sup>, a power of 5 dB and modulation amplitude of 6.3 Gpp was used to

characterise the paramagnetic species present in the sintered and grounded samples at room temperature. The EPR signal intensities were labelled as double integrated intensities (DII) calculated from the empirical relation applied by Murugaraj et al.:<sup>19</sup>

$$\text{DII} = \frac{[(\text{signal height}) \cdot (\text{signal width})]}{[(\text{sample mass}) \cdot (\text{gain}) \cdot (\text{modulation amplitude}) \cdot (\text{power})^{1/2}]} \quad (3)$$

Samples were silver painted for the electrical characterisation. Current–voltage characteristics at room temperature were obtained using a stabilised electrical source (0–220 V) and a Keithley 614 electrometer for small currents, while for large currents a multimeter was used. The electrical breakdown field was obtained at 1 mA cm<sup>-2</sup> current density. The grain voltage (*V*<sub>g</sub>) was estimated as:

$$V_g = E_r/n \quad (4)$$

where, *E*<sub>r</sub> is the breakdown voltage, and *n* is the number of grains in series of a given sample of width *L* and mean grain size *G*,

$$n = L/G \quad (5)$$

The effective barrier voltage (*V*<sub>e</sub>) for the sintered samples was

$$V_e = V_g/BG \cdot 100, \quad (6)$$

where, BG is the SnO<sub>2</sub> band gap (about 3.5eV).<sup>20</sup>

### 3. Results and discussion

Table 2 shows the densities of the sintered samples obtained through the Archimedes method. The sample composed by SnO<sub>2</sub> without additives presented a low densification after the sintering process. However, addition of Co<sub>3</sub>O<sub>4</sub>, MnO<sub>2</sub> or ZnO increased the material density. On the other hand, the Nb<sub>2</sub>O<sub>5</sub> or Sb<sub>2</sub>O<sub>3</sub> addition produced a detrimental effect on the sample density. These changes in the sample densities could be explained through modifications in the oxygen vacancy concentration, as it will be explained below.

Table 1  
Sample composition (%mol)

Sample	SnO <sub>2</sub>	Co <sub>3</sub> O <sub>4</sub>	ZnO	MnO <sub>2</sub>	Sb <sub>2</sub> O <sub>3</sub>	Nb <sub>2</sub> O <sub>5</sub>
Sn	100	–	–	–	–	–
SnCo	99.66	0.34	–	–	–	–
SnZn	99.04	–	0.96	–	–	–
SnMn	99.06	–	–	0.94	–	–
SnCoSb	99.56	0.34	–	–	0.1	–
SnCoNb	99.56	0.34	–	–	–	0.1

Table 2  
Densities of the sintered samples

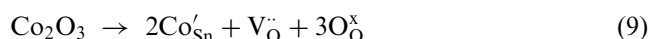
Sample	Density (g cm <sup>-3</sup> )	Relative density (%)
Sn	4.42	63.7
SnCo	6.76	97.3
SnZn	6.60	95.0
SnMn	6.74	96.9
SnCoSb	6.65	95.7
SnCoNb	6.56	94.3

From the XRD analysis only peaks corresponding to SnO<sub>2</sub> were detected, no other crystalline phase besides cassiterite (SnO<sub>2</sub>) was observed indicating that the systems were single phase within the detection precision of X-ray diffraction. XRD analysis was also used to detect the SnO<sub>2</sub> lattice distortion by the foreign ions presence. Table 3 shows the lattice parameters obtained from the Bragg equations. From the table a deformation in the lattice volume by the oxides addition was observed. These changes are influenced by the ion valence stabilised in the tin oxide lattice. An increase in the lattice volume with the Co<sub>3</sub>O<sub>4</sub>, ZnO or MnO<sub>2</sub> addition was detected. On the other hand, a diminution in the lattice volume with the Sb<sub>2</sub>O<sub>3</sub> or Nb<sub>5</sub>O<sub>5</sub> was observed from the experimental results.

In order to explain these changes, possible replace equations in the tin oxide are discussed as follows. In the Co<sub>3</sub>O<sub>4</sub> addition the possible substitution equations are:



then,



From these equations, cobalt could stabilise as Co<sup>+2</sup> (ionic radius 0.72Å)<sup>21</sup> or as Co<sup>+3</sup> (ionic radius 0.63Å).<sup>21</sup> From Table 3 cobalt addition produced an increase in the lattice volume respect to the SnO<sub>2</sub> sample. This means that cobalt must stabilise as Co<sup>+2</sup> in the SnO<sub>2</sub> lattice, because this ion has a major ionic radius (remember that Sn<sup>+4</sup> radius is 0.71 Å),<sup>21</sup> also Co<sup>+3</sup> could exist at the grain boundary and at minor concentration at grain. This result is in accordance with previous investigations employing UV–Vis DRS.<sup>10</sup> Then, from Eq. (8) an increase in the oxygen vacancy concentration with the cobalt addition was produced favouring the varistor densification.

Table 3  
SnO<sub>2</sub> lattice parameters of the sintered samples

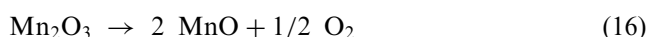
Sample	<i>a</i> (Å)	<i>c</i> (Å)	<i>V</i> = <i>a</i> <sup>2</sup> · <i>c</i> (Å <sup>3</sup> )
Sn	4.738	3.185	71.499
SnCo	4.738	3.188	71.566
SnZn	4.741	3.185	71.589
SnMn	4.744	3.185	71.680
SnCoSb	4.732	3.184	71.296
SnCoNb	4.732	3.182	71.251

In the ZnO addition, the substitution equations are:

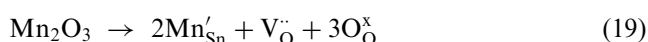
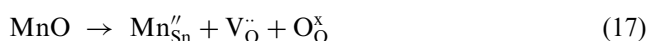


In this case, zinc ions could stabilise only as Zn<sup>+2</sup> (ionic radius 0.74Å)<sup>21</sup> and, as a consequence, the lattice volume increased (Sn<sup>+4</sup> radius 0.71 Å).<sup>21</sup>

In the MnO<sub>2</sub> addition several ions could stabilise. It is known that during the sintering process the following reactions could occur:<sup>10</sup>



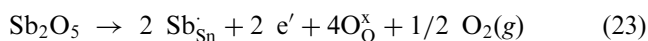
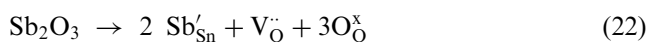
Then, the possible substitution equations are



Mn<sup>+4</sup> and Mn<sup>+3</sup> have smaller ionic radii than Sn<sup>+4</sup> (0.60, 0.66, and 0.71 Å, respectively),<sup>21</sup> but Mn<sup>+2</sup> radius is higher (0.80 Å).<sup>21</sup> From Table 3 an increases in the SnO<sub>2</sub> volume lattice with the manganese addition was observed, indicating that manganese was stabilised as Mn<sup>+2</sup> in the SnO<sub>2</sub> lattice. This result is according to previous studies by UV–Vis DRS.<sup>10</sup>

As can be seen from the above equations the addition of Co<sub>3</sub>O<sub>4</sub>, ZnO, MnO<sub>2</sub>, which stabilise as Co<sup>+2</sup>, Zn<sup>+2</sup>, and Mn<sup>+2</sup> in the lattice, produced an increase in the oxygen vacancy concentration, improving the mass transport and favouring the SnO<sub>2</sub>-based varistor densification.

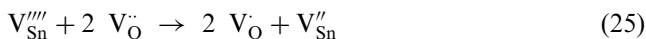
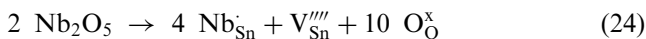
In the Sb<sub>2</sub>O<sub>3</sub> addition the possible substitution equations are:



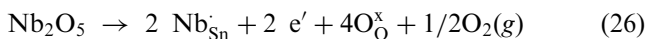
From Table 3, Sb<sub>2</sub>O<sub>3</sub> addition to SnCo system produced a diminution in the lattice volume. This diminution in the volume could not be produced by the Sb<sup>+3</sup> stabilisation (Sb<sup>+3</sup> radius is 0.76 Å)<sup>21</sup> and Sn<sup>+4</sup> radius is 0.71 Å).<sup>21</sup> According to the volume lattice data and the ionic radii, Sb<sup>+5</sup> stabilisation was produced (Sb<sup>+5</sup> radius is 0.62Å).<sup>21</sup> To explain this behaviour it is necessary to point out that Sb<sub>2</sub>O<sub>5</sub> is the stable form up to 970 °C, but Sb<sub>2</sub>O<sub>3</sub> is more stable at higher temperatures.

However, the  $\text{Sb}^{+5}/\text{Sb}^{+3}$  ratio will depend both on the temperature and on the concentration at ambient oxygen.<sup>22</sup> Then, it is possible that during the cooling process the transformation of  $\text{Sb}^{+3}$  into  $\text{Sb}^{+5}$  takes place.

In the  $\text{Nb}_2\text{O}_5$  addition the following equations could occur:



or



Experimental data were insufficient to select one of the two possible substitution equations in the  $\text{Nb}_2\text{O}_5$  addition. In both cases,  $\text{Nb}^{+5}$  has a lower ionic radius (0.69 Å)<sup>21</sup> than  $\text{Sn}^{+4}$  (0.71 Å),<sup>21</sup> and produces a diminution in the tin oxide lattice (see Table 3). From these annihilation equations of oxygen vacancies with oxygen was produced. Then, a diminution in the density samples was observed (see Table 2).

Table 4 shows the EPR double integrated intensities (DII) of the  $\text{V}_{\text{O}}^{\cdot}$  signal on sintered and grounded samples. An increase in the paramagnetic oxygen vacancy concentration with  $\text{Co}_3\text{O}_4$  or  $\text{ZnO}$  addition was observed. According to the above discussion, cobalt could stabilise as  $\text{Co}^{+2}$  and zinc as  $\text{Zn}^{+2}$  producing  $\text{V}_{\text{O}}^{\cdot}$  during lattice substitution. After that,  $\text{V}_{\text{O}}^{\cdot}$  was transformed to  $\text{V}_{\text{O}}^{\cdot\cdot}$  spending electrons. Then, an increase in the paramagnetic specie ( $\text{V}_{\text{O}}^{\cdot}$ ) was observed. On the other hand, a diminution in the paramagnetic oxygen vacancy concentration with manganese addition was produced. According to the above equations, manganese could stabilise as  $\text{Mn}^{+2}$  and an increase in oxygen vacancies should be observed. It is probable that the single line corresponding to  $\text{Mn}^{+2}$  masked the  $\text{V}_{\text{O}}^{\cdot}$  signal. This fact confirms that  $\text{Mn}^{+2}$  ions remain at the grain boundaries acting as densifying agent of  $\text{SnO}_2$  powders. Also, lines with hyperfine structure due to  $\text{Mn}^{+4}$  in the bulk were detected. The broad line corresponding to  $\text{Mn}_2\text{O}_3$ <sup>23</sup> was not observed. The notable increasing in the  $\text{V}_{\text{O}}^{\cdot}$  concentration with antimony or

niobium addition was due to the transformation of  $\text{V}_{\text{O}}^{\cdot\cdot}$  into  $\text{V}_{\text{O}}^{\cdot}$ . This transformation used the electrons generated in the lattice substitution.

Fig. 1 shows SEM microstructures of the sintered samples and Table 5 lists their mean grain sizes. Different sintered microstructures with the oxide addition were obtained. Tin oxide samples (Sn) showed a porous structure (low density), small grain size (0.5 μm) and agglomerates close to 5 μm, indicating a small sinterisation without dopant addition. In this case, the low sinterability is related to the low self-diffusion coefficient of  $\text{Sn}^{+4}$  and  $\text{O}^{-2}$  in  $\text{SnO}_2$  and to the vapour pressure of  $\text{SnO}_2$  at sintering temperatures favouring non-densifying mechanisms as evaporation–condensation.<sup>20</sup> The addition of several dopants favours the oxygen vacancies formation and allows the grain growth through a solid-state diffusion mechanism.<sup>14</sup> From Fig. 2, a high electrical conduction in sample Sn was observed. The small grain size, registered in this sample, favoured the intergranular barrier overlapping after the slow cooling process from the sintering temperature. These overlapped barriers improved the electrical conduction

Samples with zinc (SnZn) showed densities close to the theoretical density (Table 2) and an homogeneous grain microstructure with a mean grain size of 3 μm. In these samples non secondary phases were observed by SEM. Notable grain growth in these samples was produced by oxygen vacancies formation during the ions substitution (Table 5). From Fig. 2 an important diminution in the sample conductivity with  $\text{ZnO}$  addition was observed. This diminution was due to the homogeneous microstructure, and to the increase in the effective barrier voltage value due to the dopant substitution (Table 5). These barriers decreased the electrical conduction in the prebreakdown region. These samples also presented the higher breakdown electrical field (Table 5).

Samples with  $\text{Co}_3\text{O}_4$  produced samples with an intermediate conduction between Sn and SnZn, a breakdown electrical field of about 920 V/cm and a grain size range of 1–20 μm. This wide grain size distribution was caused by a non-homogeneous dopant substitution in the sample. The apparition of big grains produced a reduction in the breakdown electrical field and increased the sample conductivity. Also, a diminution in the  $V_g$  respect to sample SnZn was registered. This change could be attributed to a more effective substitution in the sample with  $\text{ZnO}$ .

Manganese addition produced an important grain growth (mean grain size 8.2 μm with grains as large as 20 μm) indicating that another sintering mechanism appears. Gouvea et al.<sup>24</sup> did not find a liquid formation by TEM. They considered that the low solubility cannot affect significantly the intrinsic disorder of  $\text{SnO}_2$  at high temperature. Consequently, they did not consider an improvement of volume diffusion due to Mn dissolution. They determined that the matter transport occurs only at the grain surfaces when the surface manganese

Table 4  
Relative EPR double integrated intensities (DII) of  $\text{V}_{\text{O}}^{\cdot}$  ( $g = 1.89$ ) for the sintered and grounded samples

Sample	DII ( $\text{V}_{\text{O}}^{\cdot}$ ) / DII ( $\text{V}_{\text{O}}^{\cdot}$ ) in sample Sn
Sn	1
SnCo	3.37
SnZn	1.23
SnMn	0.19
SnCoSb	202.6
SnCoNb	328.9

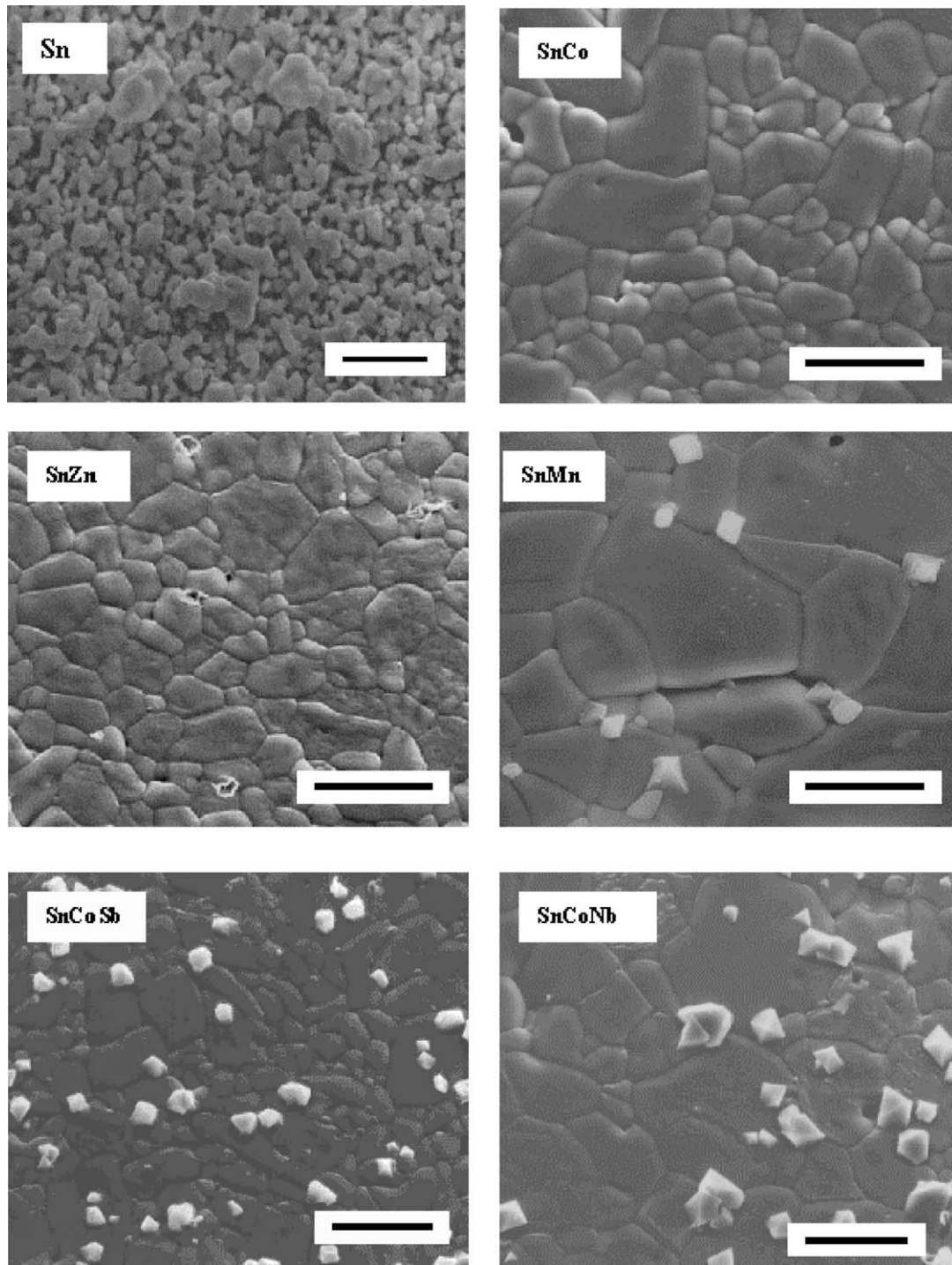


Fig. 1. SEM microstructure of the sintered samples. Bar = 10  $\mu\text{m}$ .

concentration is lower than a critical value estimated as  $5 \times 10^{-6} \text{ mol m}^{-2}$ . When the Mn surface concentrations is larger than the critical concentration the thickness of the segregation layer would be larger to provoke the diffusion in a volume localised around the grains and not only on the surface. In these samples a secondary phase at the grain boundaries was detected by SEM. Analyses performed by EDS showed that this phase has Sn and Mn

in a relation close to 1:11.5. Early papers presented the possible apparition of  $\text{Mn}_2\text{SnO}_4$  and/or  $\text{Mn}_2\text{O}_3$  phases in tin oxide varistors<sup>24</sup> but by EPR analysis the presence of  $\text{Mn}_2\text{O}_3$  particles was not detected in this study. It is probable that the secondary phase composition is close to MnO with a small quantity of  $\text{Mn}_2\text{SnO}_4$ . From Fig. 2 and Table 5 an important diminution in the electrical conductivity, a reduction in the grain voltage ( $V_g$ ) and

Table 5

Mean grain size, number of barriers, breakdown field, grain voltage and effective voltage value of the samples

Sample	Mean grain size ( $\mu\text{m}$ )	Number of barriers	Breakdown field (V/cm)	Grain voltage ( $V_g$ )	Effective barrier voltage value (%)
Sn	0.5	3000	1000	0.05	1.4
SnCo	4.8	312	920	0.44	12.6
SnZn	3.0	500	2300	0.69	20.0
SnMn	8.2	183	2000	1.64	47.0
SnCoSb	3.1	483	400	0.124	3.5
SnCoNb	6.5	231	600	0.39	11.4

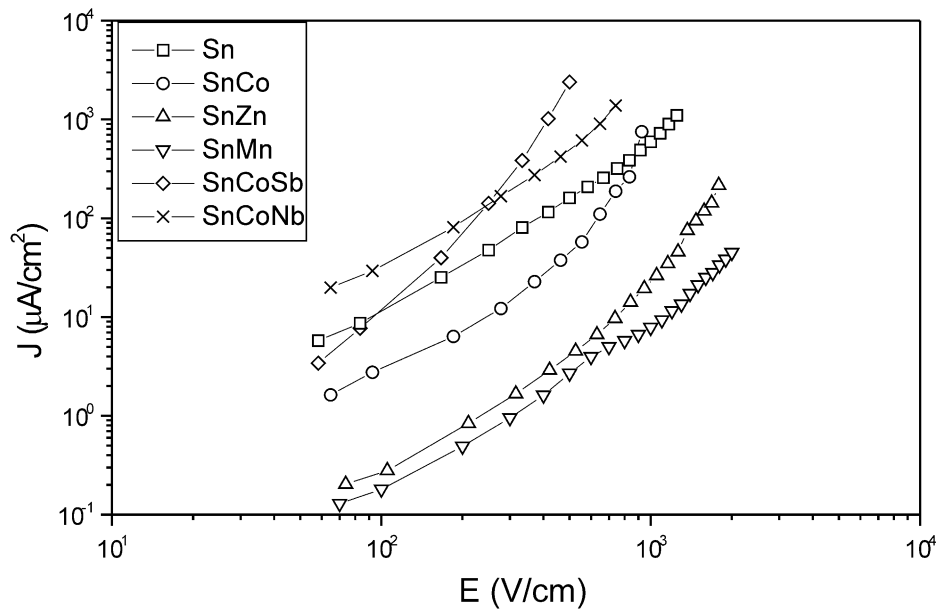


Fig. 2. Density current against applied voltage field curves.

an increasing in the breakdown electrical field were registered. The more effective barrier voltage in this sample was due to a more effective dopant substitution. Also the presence of secondary phases at the grain boundaries could influence the electrical conduction.

In samples with  $\text{Co}_3\text{O}_4$ ,  $\text{ZnO}$  or  $\text{MnO}_2$  segregated ions to the grain boundaries contributed to the potential barrier formation at the grain boundaries. These barriers were responsible of the varistor non-ohmic properties. Also, the presence of precipitated secondary phases in sample with manganese could modify the electrical behaviour.

Samples with antimony addition showed small grains (between 0.5 and 5  $\mu\text{m}$ ), and precipitated particles of a secondary phase at the grain boundaries. An analysis by EDS of the secondary phase indicated the presence of Co and Sn in a relation 1:1.1, permitting to conclude that the chemical composition of this phase is close to  $\text{CoSnO}_3$ . The notable reduction in the grain size was due to the possible effect of the secondary phase inhibiting the grain growth, and to the reduction in the total oxygen vacancy concentration by the oxygen produced in the antimony substitution [Eq. (23)], and by the cobalt solution in the secondary phase.

Samples with niobium addition showed grain sizes between 3 and 20  $\mu\text{m}$ , and the presence of a secondary phase. Analysis by EDS showed that the secondary phase was composed by Sn and Co in a relation 1:1.4, indicating that the precipitated secondary phase composition was intermediate between  $\text{CoSnO}_3$  and  $\text{Co}_2\text{SnO}_4$ . In these samples  $\text{Nb}^{+5}$  substituted  $\text{Sn}^{+4}$  in the  $\text{SnO}_2$  lattice and segregated cobalt at the interface forming secondary phase particles.

On the other hand,  $\text{Sb}_2\text{O}_3$  or  $\text{Nb}_2\text{O}_5$  addition produced an increment in the samples conductivity and a diminution in the breakdown electrical field (Table 5), due to electrons produced in the ion substitution [see Eqs. (23) and (26)]. Moreover, samples with  $\text{Sb}_2\text{O}_3$  presented small grains (between 0.5 and 5  $\mu\text{m}$ ) which favoured the intergranular barriers overlapping.

#### 4. Conclusions

The experimental results lead to the following conclusions.

1. From the lattice volume distortion and the substitution equations it is possible to conclude that cobalt, zinc and manganese were stabilised as  $\text{Co}^{+2}$ ,  $\text{Zn}^{+2}$ ,  $\text{Mn}^{+2}$  in  $\text{SnO}_2$  varistors, increasing the oxygen vacancy concentration.
2. The increase in the oxygen vacancy concentration could be responsible for an increasing in the densification and grain growth.
3. Manganese addition provoked an important grain growth and the formation of precipitated particles with a composition close to  $\text{MnO}$ . Also, manganese was segregated at the grain boundaries and the matter transport concerned the solid/gas interface and the grain boundaries.
4. Niobium or antimony addition to samples with cobalt favoured the formation of particles of a composition close to  $\text{CoSnO}_3$  with antimony addition or intermediate between  $\text{CoSnO}_3$  and  $\text{Co}_2\text{SnO}_4$  with niobium addition. This secondary phase and the annihilation of the oxygen vacancy concentration decreased the grain growth of the samples.
5.  $\text{Co}_3\text{O}_4$ ,  $\text{ZnO}$ , and  $\text{MnO}_2$  improved the current density vs. electrical field characteristics due to the increasing in oxygen vacancies concentration and to the substitution of tin ions by added metal ( $\text{M}'_{\text{Sn}}$ ,  $\text{Mn}'_{\text{Sn}}$ ).

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